

# **Control Theory Applications**

## **Balancing Scooters**

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# Inverted Pendulum

- Hoover boards, balancing scooters, wiziwig scooters...etc. are forms of Balancing Inverted Pendulums



Short Video, Balancing Scooter

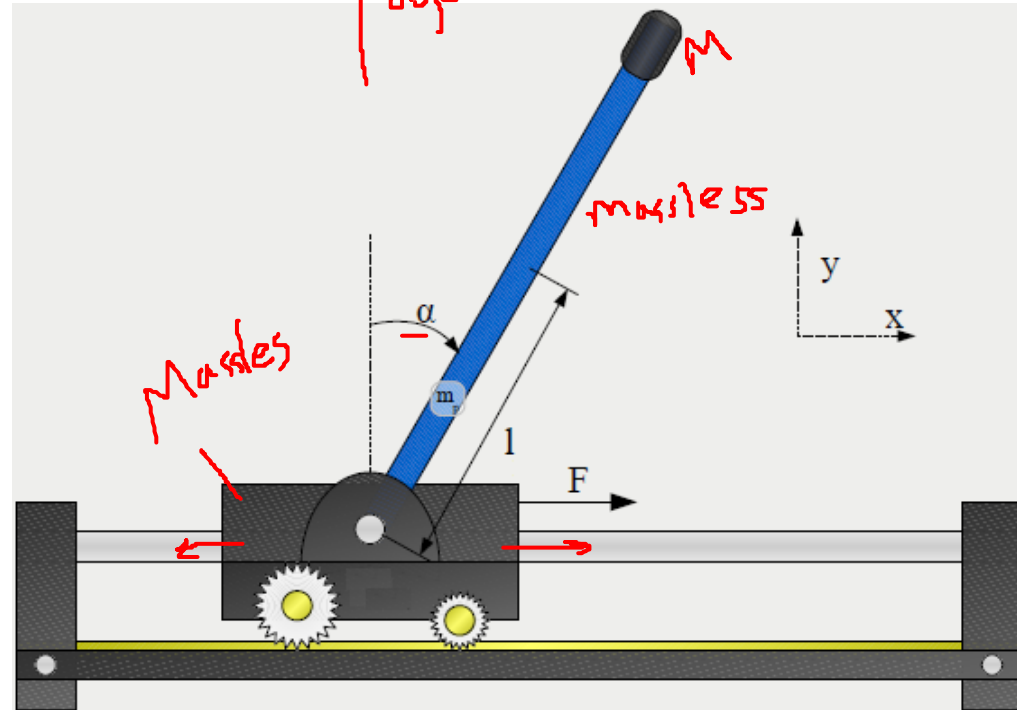


# Inverted Pendulum

- Consider the balancing of an inverted pendulum problem as shown by the diagram
- Suppose that the cart is massless and it moves on a frictionless rails
- Assuming a first order motor that generates a traction force

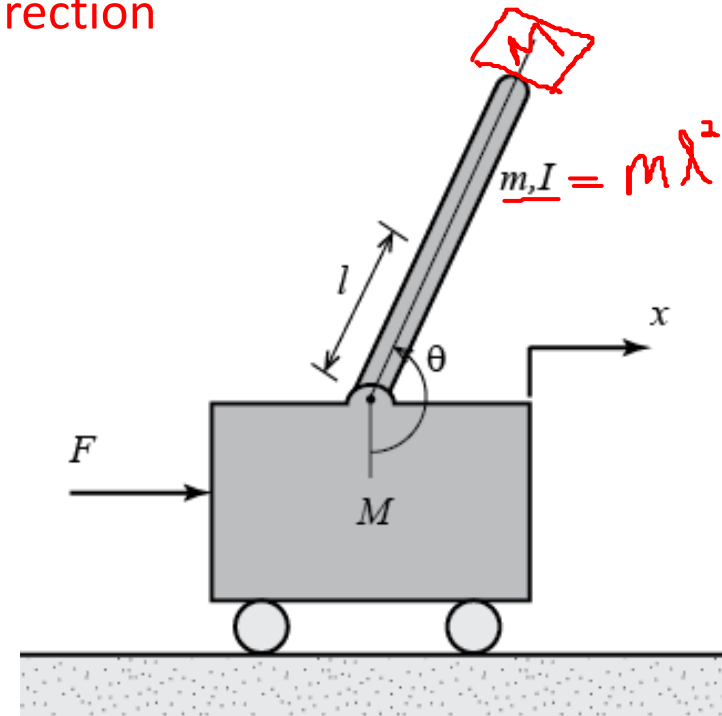
$$\frac{F(S)}{V(S)} = \frac{C}{\tau S + 1}$$

- Where
  - C is a motor constant
  - $\tau$  is a motor time constant
  - V is a motor input voltage



# Inverted Pendulum

- First let us draw a sketch of the physical model as shown in the diagram, with the following assumptions:
  - The person will be modeled as a rod with mass  $m$  and mass moment of inertia  $I$
  - The rod's center of gravity is located in the middle
  - The rod is pivoted to a massless cart as shown
  - The cart can move back and forth in the  $x$ -direction
  - The motor generates a varying force  $F$



# Inverted Pendulum

- From the free body diagram of the cart

- Summation of forces in the x-direction

$$\underline{M\ddot{x}} + \underline{b\dot{x}} + N = F$$

- Assuming massless cart and frictionless ground surface

$$N = F$$

- From the free body diagram of the rod

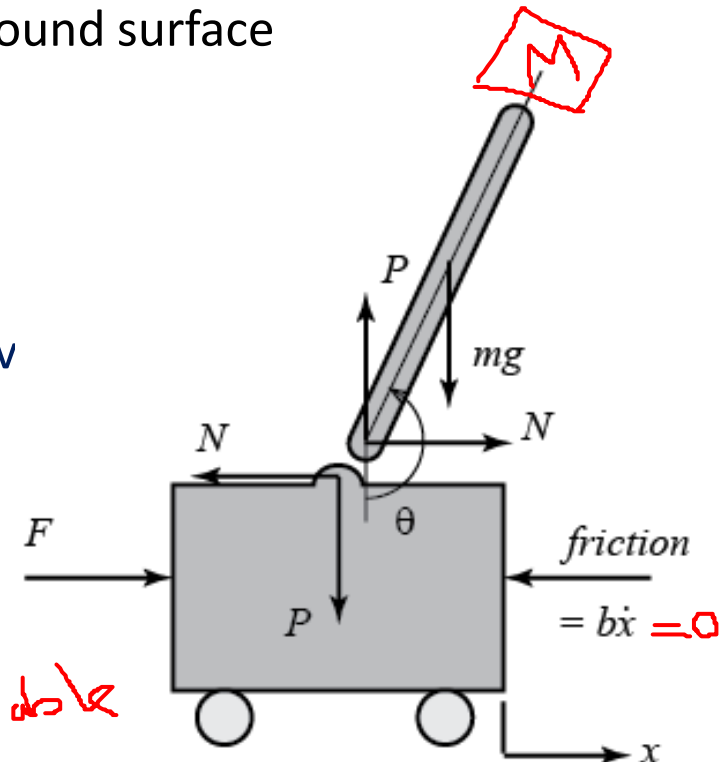
- Taking summation of torques about the piv

$$T = Fl = I\ddot{\alpha} - mgl\sin(\alpha)$$

$\sin(\alpha) \approx \alpha$  for a small vertical angle

$$T = Fl \text{ Torque}$$

show the system is unstable



# Inverted Pendulum

- The system transfer function

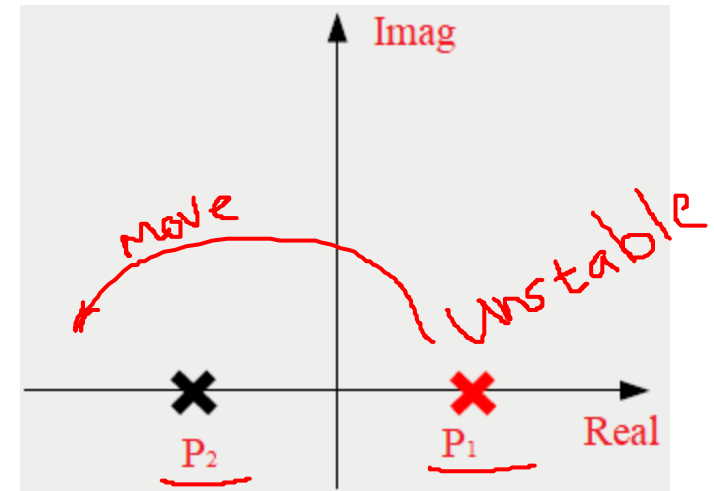
$$G(S) = \frac{\alpha(S)}{T(S)} = \frac{1}{\underline{IS^2 - mgl}}$$

- The characteristic Equation

$$D(S) = IS^2 - mgl = 0$$

$$P_{1,2} = \pm \sqrt{\frac{mgl}{I}}$$

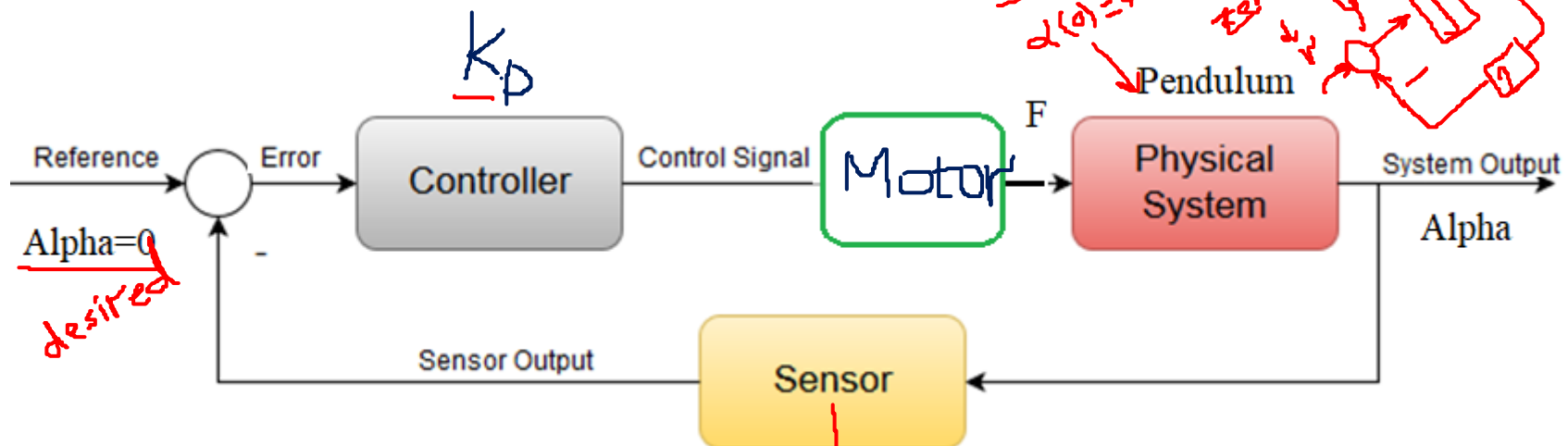
- The inverted pendulum is unstable



# Inverted Pendulum

- Stabilization using a P-Controller
  - The closed loop transfer function

$$\frac{\alpha(s)}{\alpha_d(s)} = \frac{K_p \frac{C}{\tau s + 1} \frac{1}{IS^2 - mgl}}{1 + K_p \frac{C}{\tau s + 1} \frac{1}{IS^2 - mgl}}$$



$$\frac{\alpha(S)}{\alpha_d(S)} = \frac{K_p \frac{C}{\tau S + 1} \frac{1}{IS^2 - mgl}}{1 + K_p \frac{C}{\tau S + 1} \frac{1}{IS^2 - mgl}}$$

✓  $\frac{\alpha(S)}{\alpha_d(S)} = \frac{K_p C}{(\tau S + 1)(IS^2 - mgl) + K_p C}$  type equation here.

$$D(S) = (\tau S + 1)(IS^2 - mgl) + K_p C = 0$$

$$= \tau I S^3 + IS^2 - mgl \tau S - K_p C - mgl = 0$$

$S^3$	$\tau I$	$-mgl \tau$
$S^2$	$I$	
$S$	$h_1$	$K_p$
$S^0$	$h_2$	

$$h_1 = \frac{1}{I} (K_p \tau I + I \cdot)$$

$$h_2 = K_p > 0$$

✓  $K_p > 0$

Why  $K_p$  alone cannot stabilize the pendulum?

$$u = K_p e = -K_p \alpha$$

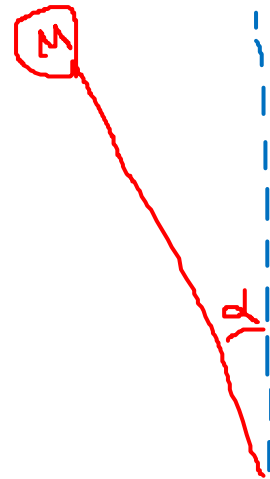
$$e = \theta_p - \alpha = -\alpha$$

Idea

$$u = K_p e + K_D \frac{de}{dt}$$

Proportional + Derivative

CO: Reaction based  $\alpha + \dot{\alpha}$



PD

