

Control Theory Applications

Balancing Scooters

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Inverted Pendulum

- Hoover boards, balancing scooters, wizwig scooters...etc. are forms of Balancing Inverted Pendulums



Short Video, Balancing Scooter

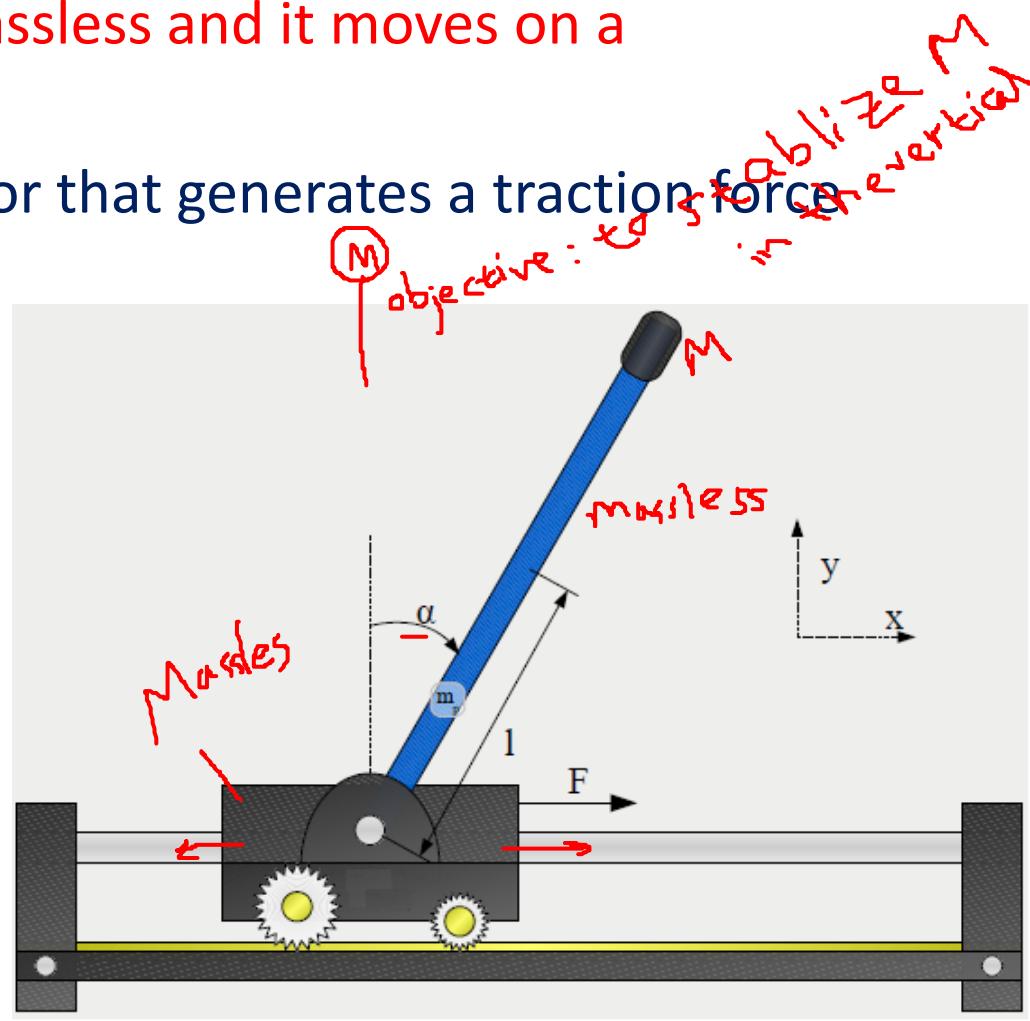


Inverted Pendulum

- Consider the balancing of an inverted pendulum problem as shown by the diagram
- Suppose that the cart is massless and it moves on a frictionless rails
- Assuming a first order motor that generates a traction force

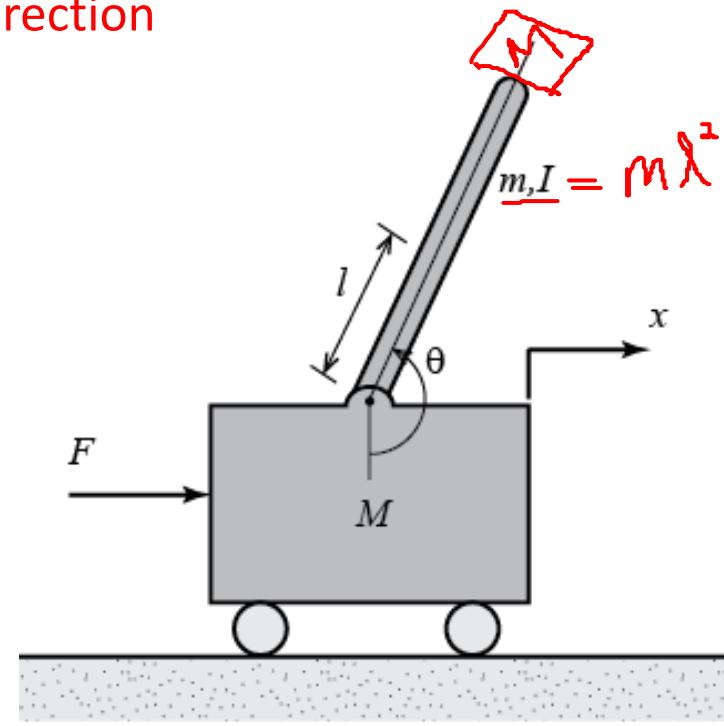
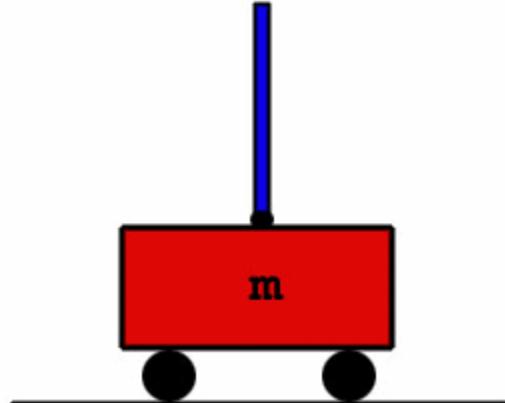
$$\frac{F(S)}{V(S)} = \frac{C}{\tau S + 1}$$

- Where
 - C is a motor constant
 - τ is a motor time constant
 - V is a motor input voltage



Inverted Pendulum

- First let us draw a sketch of the physical model as shown in the diagram, with the following assumptions:
 - The person will be modeled as a rod with mass m and mass moment of inertia I
 - The rod's center of gravity is located in the middle
 - The rod is pivoted to a massless cart as shown
 - The cart can move back and forth in the x -direction
 - The motor generates a varying force F



Inverted Pendulum

- From the free body diagram of the cart

- Summation of forces in the x-direction

$$\underline{M\ddot{x}} + \underline{b\dot{x}} + N = F$$

- Assuming massless cart and frictionless ground surface

$$N = F$$

- From the free body diagram of the rod

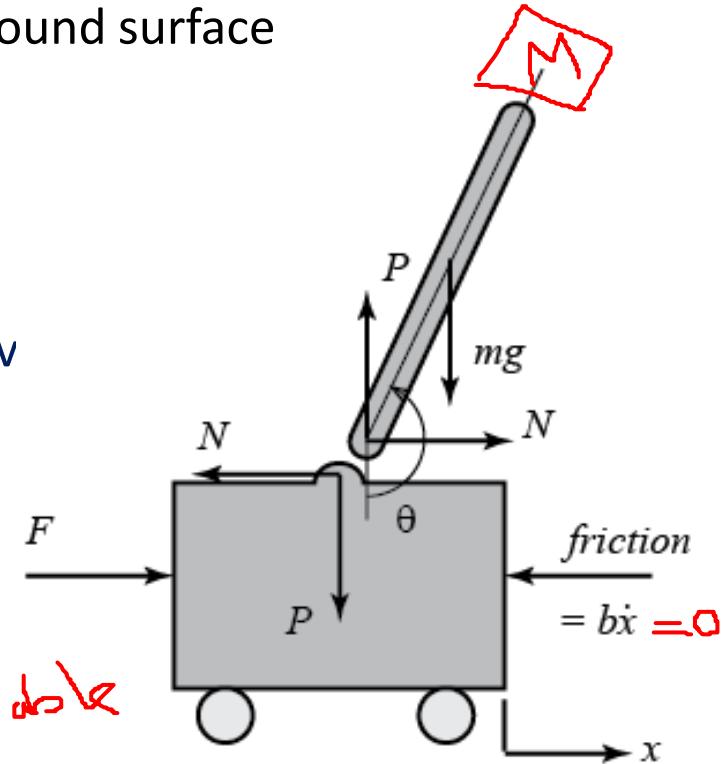
- Taking summation of torques about the pivot

$$T = Fl = I\ddot{\alpha} - mglsin(\alpha)$$

$\sin(\alpha) \approx \alpha$ for a small vertical angle

$$T = Fl \text{ Torque}$$

Show the system is unstable



Inverted Pendulum

- The system transfer function

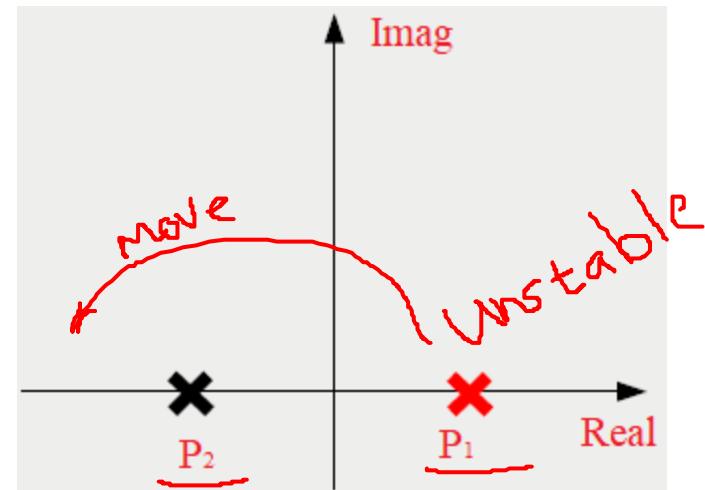
$$G(S) = \frac{\alpha(S)}{T(S)} = \frac{1}{IS^2 - mgl}$$

- The characteristic Equation

$$D(S) = IS^2 - mgl = 0$$

$$P_{1,2} = \pm \sqrt{\frac{mgl}{I}}$$

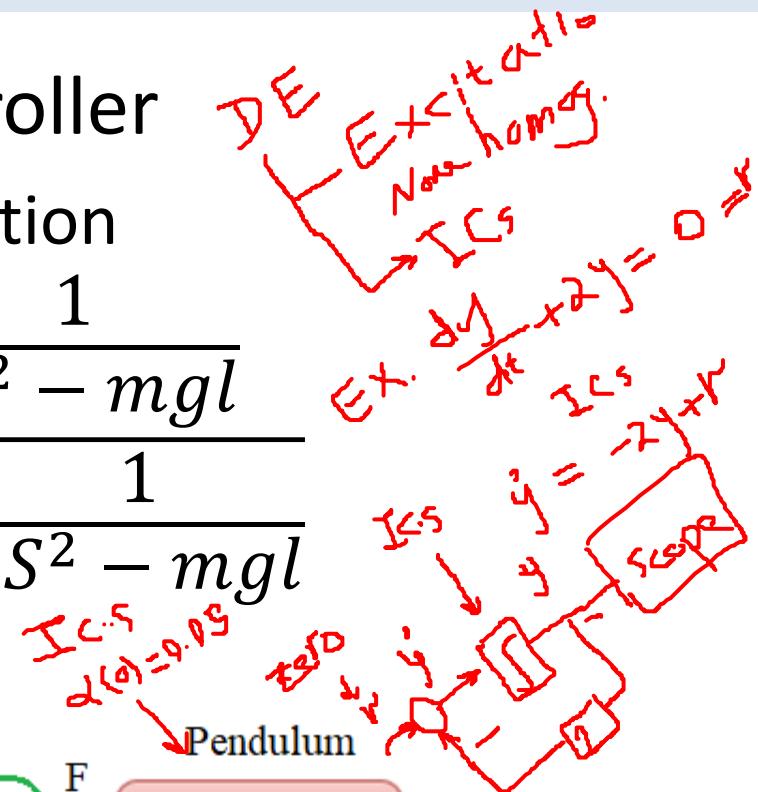
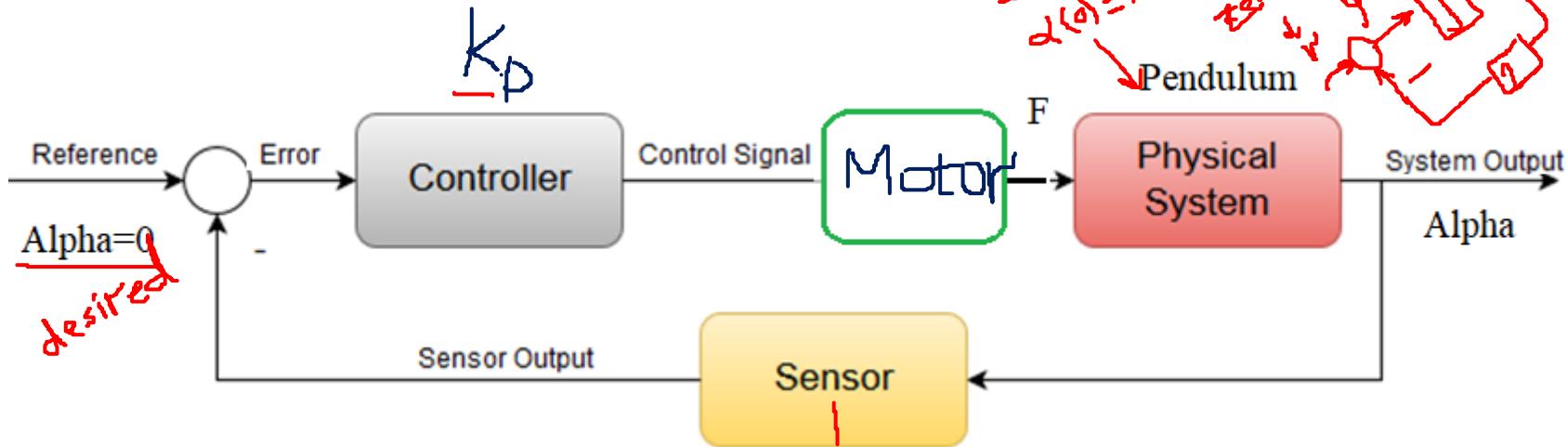
- The inverted pendulum is unstable



Inverted Pendulum

- Stabilization using a P-Controller
 - The closed loop transfer function

$$\checkmark \frac{\alpha(S)}{\alpha_d(S)} = \frac{K_p \frac{C}{\tau S + 1} \frac{1}{IS^2 - mgl}}{1 + K_p \frac{C}{\tau S + 1} \frac{1}{IS^2 - mgl}}$$



$$\frac{\alpha(S)}{\alpha_d(S)} = \frac{K_p \frac{C}{\tau S + 1} \frac{1}{IS^2 - mgl}}{1 + K_p \frac{C}{\tau S + 1} \frac{1}{IS^2 - mgl}}$$

✓ $\frac{\alpha(S)}{\alpha_d(S)} = \frac{K_p C}{(\tau S + 1)(IS^2 - mgl) + K_p C}$ See equation here.

$$D(S) = (\tau S + 1)(IS^2 - mgl) + K_p C = 0$$

$$= \tau I S^3 + IS^2 - mgl \tau S + K_p C - mgl = 0$$

$$\begin{matrix} S^3 & \cancel{\tau I} & -mgl\cancel{\tau} \\ S^2 & \cancel{I} & \cancel{mgl} \\ S & \cancel{\frac{I}{\tau}} & \cancel{\tau} \\ S^0 & \cancel{\tau} & \cancel{\tau} \end{matrix}$$

$$-mgl\cancel{\tau}$$

$$h = \frac{1}{I} (K \cancel{\tau} I + I \cdot)$$

$$h_2 = k_p > 0$$

?

✓ $k_p < 0$

Why K_p alone cannot stabilize the pendulum?

$$u = K_p e = K_p \alpha$$

$$e = \bar{e}_p - \alpha = -\alpha$$

Idea

$$u = K_p e + K_D \frac{de}{dt}$$

Proportional + Derivative

CD: Reaction based α +
" " " $\ddot{\alpha}$



PD

