

Q1) Based on your understanding of the course answer the following

(10 Marks)

1. An open feed water heater used in regenerative Rankine cycle receives bled steam from the turbine at 2 MPa and 275 °C to heat the feed water from the condenser at 100 °C, 2 MPa and rate of 20 kg/s. The exit of the OFWH is saturated liquid. Calculate the mass flow rate of the bled steam. Show calculation steps.

Take the OFWH as control volume

$$\dot{m}_6 h_6 + (\dot{m} - \dot{m}_6) h_2 = \dot{m} h_3$$

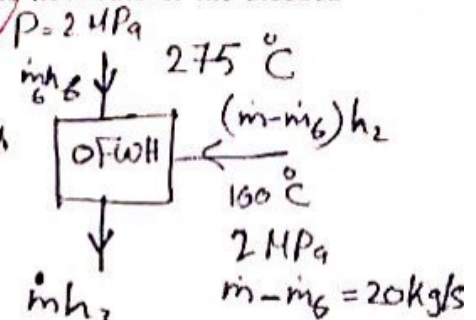
$$y h_6 + (1-y) h_2 = h_3$$

$$\frac{\dot{m}_6}{\dot{m}} = y = \frac{h_3 - h_2}{h_6 - h_2}$$

$$T = 275^\circ\text{C} \quad h = 2903.3 \text{ kJ/kg}$$

$$T = 300^\circ\text{C} \quad h = 3024.2 \text{ kJ/kg}$$

state 6 is superheated at 2 MPa



2. Write down the chemical formula for the following refrigerants

R11

1-1=0

Cl-C(F)(Cl)-F

CCl3F

C2HCl2F3

R123

2-1=1

F-C(F)(F)-F

H-C(F)(F)-F

$$h_6 = 2963.75 \text{ kJ/kg}$$

$$h_2 = h_f @ 100^\circ\text{C} = 419.17 \text{ kJ/kg}$$

$$h_3 = 908.47 \text{ kJ/kg}$$

3. Why and in which device cooling water is required for in Ammonia absorption refrigeration cycle?

in the absorber, in order to dissolve NH_3 into H_2O the absorber must be cooled. (because it is an exothermic reaction)

4. What is the function of rectifier in Ammonia absorption cycle? What is the difference between it and flash chamber in regeneration cycle?

the rectifier separates H_2O from NH_3 and allow NH_3 to enter the condenser and returns H_2O to the generator. Flash chamber is used for separation in liquids but rectifier is used for gases.

5. State TWO problems with Carnot refrigerator cycle?

① the inlet of the compressor is wet mixture. compressors can't deal with wet mixture

② the inlet of the turbine is saturated liquid. the turbine cannot allow the liquid to expand largely

6. Consider a heat pump that operates on the ideal vapor compression refrigeration cycle with R-134a as the working fluid flowing at rate 0.193 kg/s between the pressure limits of 0.3 and 1.2 MPa. Using the P-H chart find:

The enthalpies at all points: $h_1 = 300 \text{ kJ/kg}$

$h_2 = 328 \text{ kJ/kg}$

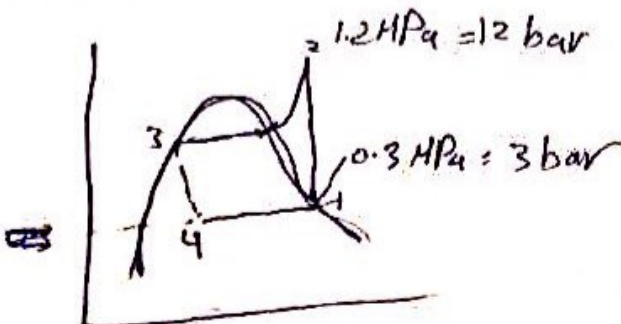
$h_3 = 165 \text{ kJ/kg}$

$h_4 = 165 \text{ kJ/kg}$

The quality of the mixture at the evaporator inlet is nearly = 32 %

The heating load for this cycle is = kW = 8.94 Tonnes

The coefficient of performance is =



$$\dot{m}_R (h_2 - h_3)$$

$$0.193 (328 - 165)$$

$$31.459 \text{ kW}$$

$$31.459 \text{ kJ/s} \cdot \frac{60 \text{ s}}{1 \text{ min}}$$

$$1887.54 \text{ kJ/min}$$

$$211 \text{ kJ/min}$$

allow the liquid to expand largely (in order to cool the liquid because liquids are incompressible)

Q2) Based on Gas Mixture Chapter answer the following

A mixture of ideal gases consists of 4 kg of Nitrogen (N_2) and 6 kg of Carbon Dioxide (CO_2) at a pressure of 0.1 MPa and a temperature of $25^\circ C$.

Find :

- (i) The mass and mole fraction of each constituent (m_i and y_i),
- (ii) The molecular weight of the mixture (M_{mix}),
- (iii) The gas constant of the mixture (R_{mix}),
- (iv) The partial pressure for each component (P_i),
- (v) The volume and density of the mixture, and
- (vi) The c_p and c_v of the mixture.
- (vii) If the mixture is heated at constant volume to $50^\circ C$, find the changes in internal energy and entropy of the mixture.
- (viii) If the mixture is compressed adiabatically to 0.25 MPa find the final temperature and work done.

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Q3) Based on Refrigeration cycles' Chapter answer the following

A vapor-compression refrigeration system circulates Refrigerant 134a at a rate of 6 kg/min. The refrigerant enters the compressor at $-10^\circ C$, 1.4 bar, and exits at 7 bar. The isentropic compressor efficiency is 67%. There are no appreciable pressure drops as the refrigerant flows through the condenser and evaporator.

The refrigerant leaves the condenser at 7 bar, $24^\circ C$. Ignoring heat transfer between the compressor and its surroundings, determine

- (a) The coefficient of performance and its theoretical maximum value.
- (b) The refrigerating capacity, in tons. (Define the word "Tonne" of refrigeration)
- (c) The rates of exergy destruction in the compressor and expansion valve, in kW.
- (d) The second law efficiency of the cycle.
- (e) The cost of running this cycle for one month, 8 hours per day with electricity cost 0.8 JD/kW-hr.

Take $T_o = 21^\circ C$, $P_o = 1$ bar.

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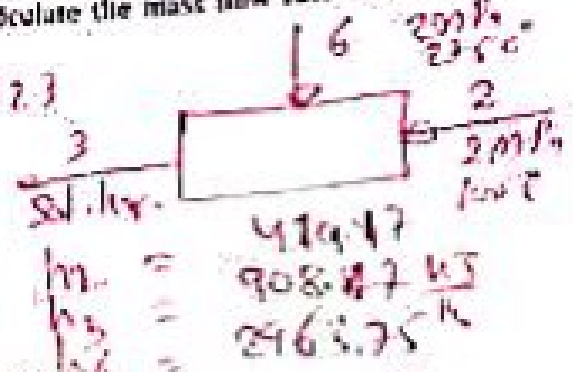
(10 Marks)

Q1) Based on your understanding of the course answer the following

1. An open feed water heater used in regenerative Rankine cycle receives bled steam from the turbine at 2 MPa and 275 °C to heat the feed water from the condenser at 100 °C, 2 MPa and rate of 20 kg/s. The exit of the OFWH is saturated liquid. Calculate the mass flow rate of the bled steam. Show calculation steps.

$$Y = \frac{h_3 - h_2}{h_6 - h_2} = 0.1923$$

$$\dot{m}_6 = 3.845 \text{ kg/s}$$



2. Write down the chemical formula for the following refrigerants
R11 CCl_3F R123 C_2HClF_3

3. Why and in which device cooling water is required for in Ammonia absorption refrigeration cycle?

Absorber to dissolve NH_3 in water.

4. What is the function of rectifier in Ammonia absorption cycle? What is the difference between it and flash chamber in regeneration cycle?

Rectifier → removes NH_3 & H_2O vapour
Flash chamber → removes H_2O vapour before pump!

5. State TWO problems with Carnot refrigerator cycle?

Check book

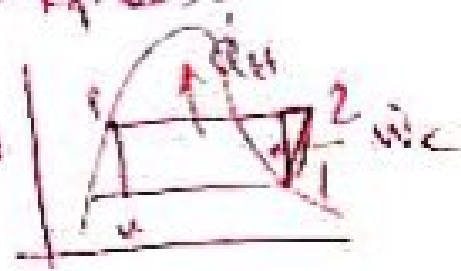
6. Consider a heat pump that operates on the ideal vapor compression refrigeration cycle with R-134a as the working fluid flowing at rate 0.193 kg/s between the pressure limits of 0.8 and 1.2 MPa. Using the P-h chart find:

The enthalpies at all points: $h_1 = 203$ $h_2 = 33$ $h_3 = 106$ $h_4 = 106$
The quality of the mixture at the evaporator inlet is nearly 30%
The heating load for this cycle is = 4.65 kW
The coefficient of performance is = 6.88

$$\dot{Q}_{\text{heating}} = 211 \frac{\text{kJ}}{\text{min}}$$

$$= 2663.4 \text{ W}$$

$$\dot{Q}_{\text{heating}} = 31.845 \text{ kW}$$



Q2) $P_{\text{mix}} = 100 \text{ kPa}$, $T_{\text{mix}} = 25^\circ \text{C}$

	m	M	N _i	m_i	y_i	Q_i	mc. Q_i
N_2	4	28	0.14285	0.4	0.5116	4.2039	
CO_2	6	44	0.13636	0.6	0.4813	0.546	
Σ	10 kg		0.27922	1	1		

$$M = \frac{m}{M}, \quad R_{\text{mix}} = \frac{R_u}{M_{\text{mix}}} = \sum m_i \cdot R_i$$

(2) $M_{\text{mix}} = \frac{M_{\text{mix}}}{M_{\text{mix}}} = 35.514 \frac{\text{kg}}{\text{kmol}}$

(3) $R_{\text{mix}} = 0.23214 \frac{\text{kJ}}{\text{kg} \cdot \text{K}}$

(4) $\frac{P_i}{P_{\text{tot}}} = \frac{y_i}{1} \Rightarrow P_{CO_2} = 48.113 \text{ kPa}$
 $P_{N_2} = 51.16 \text{ kPa}$
 $R_{CO_2} = 0.1889$
 $R_{N_2} = 0.2218$

(5) $Q_{\text{Pmix}} = \sum m_i \cdot Q_i = 0.4232 \frac{\text{kJ}}{\text{kg} \cdot \text{K}}$

$\therefore Q_{\text{Pmix}} = -R_{\text{mix}} + Q_{\text{Pmix}} = 0.69106$

$K_{\text{mix}} = (Q/P)_{\text{mix}} = 1.736$

(6) $(PV = nRT)_{\text{mix}} \Rightarrow V_{\text{mix}} = \frac{M_{\text{mix}} \cdot P_{\text{mix}} \cdot T_{\text{mix}}}{P_{\text{mix}}}$
 $= \frac{N_{\text{mix}} \cdot R_u \cdot T_{\text{mix}}}{P_{\text{mix}}}$

(7) $Q_{\text{in}} = m \cdot C_v \cdot \Delta T$

$= 172.765 \text{ kJ}$

(8) $\frac{\Delta U}{\Delta S} = m C_v \ln \frac{T_2}{T_1} + m C_p \ln \frac{P_2}{P_1}$
 $= 0.5569 \frac{\text{kJ}}{\text{kg}}$
 $S_{\text{mix}} = \frac{m \cdot C_p}{T_{\text{mix}}} = 6.928 \text{ kJ/kg} \cdot \text{K}$
 $1.4455 \frac{\text{kJ}}{\text{kg} \cdot \text{K}}$

(9) $T_2 = T_1 \left(\frac{P_2}{P_1} \right)^{\frac{\gamma}{\gamma-1}} \Rightarrow T_2 = 325.23 \text{ K}$
 $W = m C_v (T_2 - T_1) = 5.56 \text{ kJ}$

$$b) \dot{Q}_L = \dot{m}_R (h_1 - h_u) = 16.138 \text{ kW}$$

$$= 4.6 \text{ Tonn}$$

$$c) \dot{X}_{\text{dest } 1-2} = \dot{m}_R T_0 (s_2 - s_1)$$

$$= 0.14294 (1.02 - 0.9229)$$

$$= \underline{1.4 \text{ kW}}$$

$$\dot{X}_{\text{dest } 3-4} = \dot{m}_R T_0 (s_4 - s_3)$$

$$= 0.14294 (0.38473 - 0.51975)$$

$$= \underline{0.555 \text{ kW}}$$

$$d) \eta_{II} = \frac{COP_R}{COP_{R_{max}}} = \frac{3.104}{5.6} \times 100\%$$

$$= 55.5\%$$

$$e) \dot{X}_{\text{dest } Win} \quad \dot{X}_{Q_c} = 2.5245$$

$$\text{Cost} = \text{time} \times \text{fuel} \times \text{Win}$$

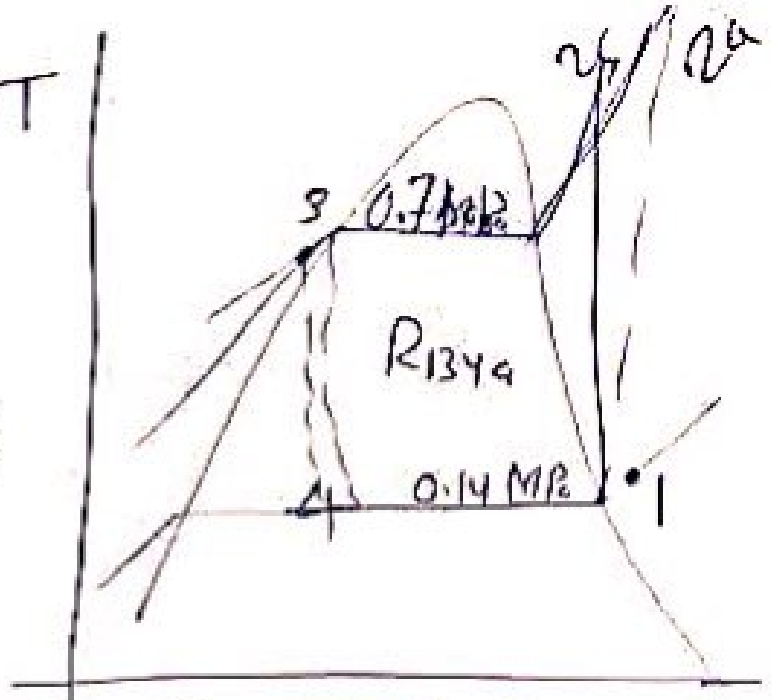
$$= \frac{8 \text{ hrs}}{\text{day}} \times \frac{30 \text{ days}}{\text{month}} \times \frac{0.8 \text{ T/D}}{\text{kg} \times \text{kg}} \times \frac{15.183}{\text{kg}}$$

$$= 948.4 \text{ ID/month}$$

Q3) $\dot{m}_R = 6 \text{ kg/min}$ T
 $\omega = 0.1 \text{ rev/s}$

1) -10°C , 1.4 bar
 $= 0.14 \text{ MPa}$

Superheated.
 $h_1 = 246.36 \frac{\text{kJ}}{\text{kg}}$
 $s_1 = 0.9724 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$



2) $\eta_c = 67\%$, $s_2 = s_1$, $P_2 = 0.7 \text{ MPa} \Rightarrow h_2 = 281.489$
 $\therefore h_{2a} = 298.343$, $s_{2a} = 1.02 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$

3) 7 bar , 24°C Subcooled
 0.2 MPa

$\therefore h_3 = h_f @ 24^\circ\text{C} = 84.98$
 $s_3 = s_f @ 24^\circ\text{C} = 0.31958$

4) $h_4 = h_3 = 84.98$
 $= x_4 h_g + (1-x_4) h_f$

$\therefore x_4 = 0.273$

$s_4 = s_f + x_4 s_{fg} = 0.338473$

A) $\text{COP}_R = \frac{h_1 - h_4}{h_{2a} - h_1} = \frac{246.36 - 84.98}{298.343 - 246.36} = 3.104$

$\text{COP}_{\text{min}} = \frac{T_L}{T_H - T_L} = \frac{-18.22 + 273}{2669 - (-18.22)} = 5.592$