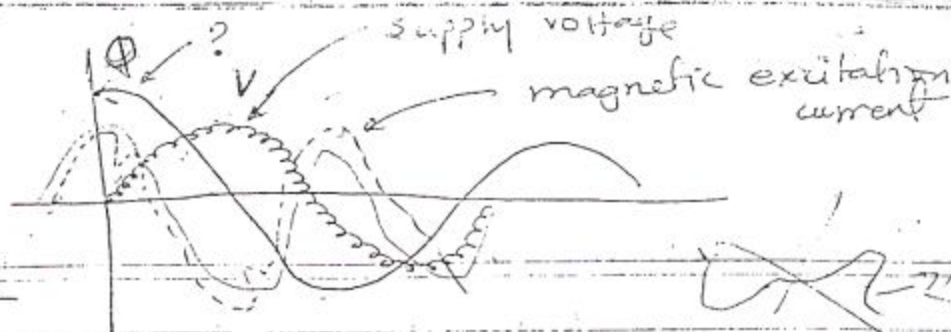


Regulator



$$V_g = \frac{V_{max} - V_{min}}{V_{min}}$$

o st ; $V = (3-5\%)$ Reg. (احمال)

o one of the following is non-self start motor :-
Synchronous (المحركات)

o أي ماتور يستخدم لتحسين ال PF في الشبكة
المحركات Induction synchronous (منه)

5 أنواع مواتر دس طبقه التحكم بالتيار والسرعة
بجودة عالية

DC series voltage

DC sep-excited → Field weakening, R_a , E_a

Induction → (phase sequence) diverst,

Synchronous → "

o type of following transformer ?



Core



Shell

power supply

o VARIAC = variable AC transformer

o for transformer experiment:-

V_1 & V_2 is leading ϕ
lagging ϕ
in-phase $\checkmark$

ϕ lag V by 90°

V_c in phase with ϕ

- ϕ Lag V_1 by 90°

(Proof)

$\Rightarrow \phi$ and i are in phase

$$\left(iN = \phi R_m \right. \\ \Rightarrow \phi = i \left(\frac{N}{R_m} \right) \rightarrow (\text{constant})$$

- ϕ Lead E_1 by 90° .

$$* V_1 \approx 4.44 N_1 f \phi_m$$

$$E_1 = 4.44 N_1 f \phi_m$$

$$a = \frac{N_1}{N_2} \equiv \text{Turns Ratio.}$$

$$a_T = \frac{E_1}{E_2} \approx \frac{V_1}{V_2} \equiv \text{Transformation ratio}$$

$$\text{in general } a_T = a.$$

* if the load is inductive (Lag PF) $\Rightarrow I_2 \angle -$
 " " " " capacitive (Lead) $\Rightarrow I_2 \angle +$
 " " " " resistive (neutral) $\Rightarrow I_2 \angle 0$

$$S_L = V_2 \times I_2^* \\ S_L = P \pm jQ \\ = \sqrt{P^2 + Q^2} \angle \tan^{-1} \frac{Q}{P} \\ \text{-if } jQ \text{ is +ve} \\ \Rightarrow \text{Inductive load.} \\ \text{-if } jQ \text{ is -ve} \\ \Rightarrow \text{Capacitive load}$$

efficiency

$$\eta = \frac{P_o}{P_{in}} \times 100\%$$

$$\eta = \frac{P_o}{P_{in}} = \frac{V_2' I_2' \cos \phi_{out}}{V_2' I_2' \cos \phi_{out} + P_{cu} + P_c} \\ I_2'^2 R_{eq}$$

- η depend on

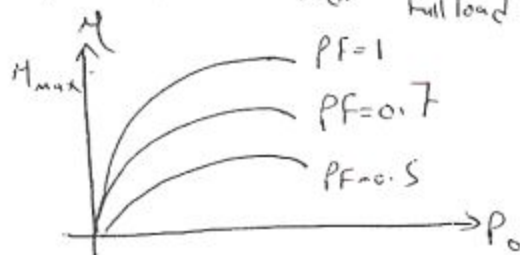
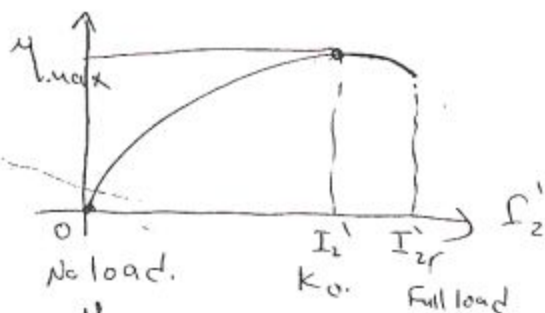
- ① Load power or current (I_2').
- ② Load PF.

$$\eta_{max} = \frac{k_0 S_r \cos \phi_{out}}{k_0 S_r \cos \phi_{out} + k_0^2 P_{cu} + P_c}$$

$$\eta = \frac{k S_r \times PF_{out}}{k S_r \times PF_{out} + k^2 P_{cu} + P_c}$$

- if $k = \text{constant}$

max. η is at $PF_{out} = 1$ (Unity PF)



consider the max. possible efficiency (T)

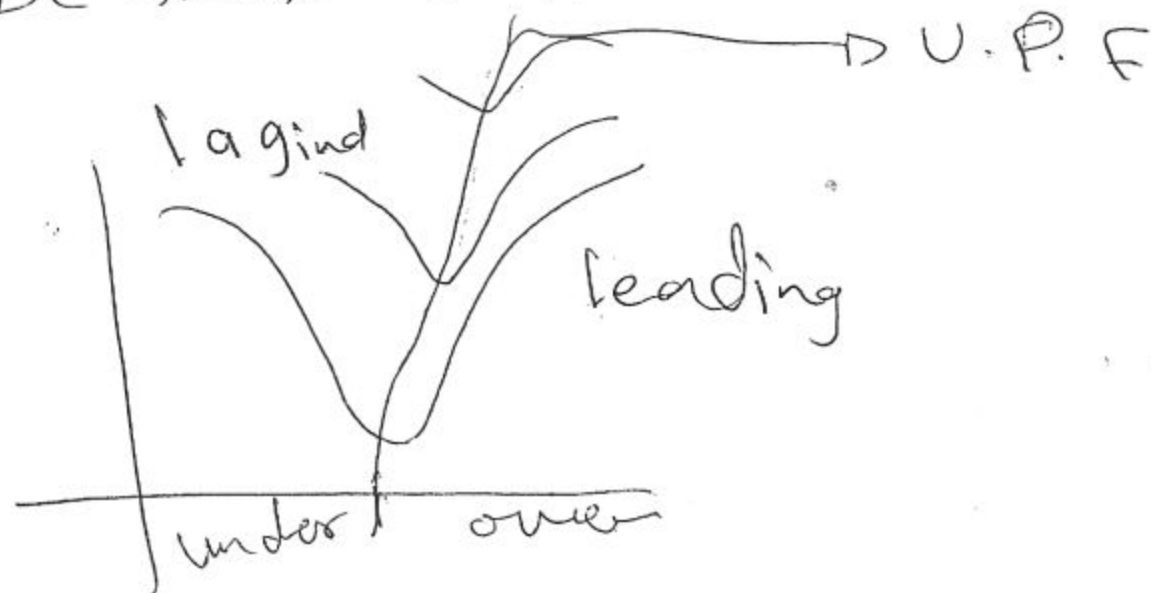
DC-series $\rightarrow$ Armature voltage control

DC-separately excited $\rightarrow$ field weakening method
synch.

~~Induction~~ $\rightarrow$ variable freq control.

~~induction~~
~~Synchronous~~ $\rightarrow$ adding R_{ext} for wound rotor

DC-shunt $\rightarrow$ Armature resistance control





V-curve of synchronous

lead or lag $\leftarrow$ pf = 1 $\rightarrow$ $\leftarrow$ over or under excitation $\leftarrow$

O.C.T

$I_o \equiv (1-5)\% I_r$ rated

الموتور على الفاراد

I_c in phase with E_2
 I_m lag E_1 by 90°

$\frac{V_{sc}}{V_r} \times 100\% = 5-13\% \rightarrow V_{sc} = (5-13)\% V_r$

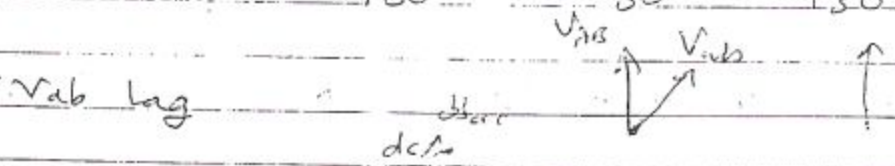
$I_o(r) = (1-5)\% I_r$

$I_o(sc) = \frac{V_{sc}}{V_r} (1-5)\% I_r$

$I_o(sc) = \frac{0.005}{0.004} I_r$

$\frac{5}{100} \times \frac{3}{100} \times \frac{5}{100} \times 10$

Groups	1	2	3	4
	$\downarrow$	$\downarrow$	$\downarrow$	$\downarrow$
	0°	180°	-30°	$+30^\circ$



mechanical Rectifier $\rightarrow$ commutator $\rightarrow$ Rect of Rectifier?

Generator $\rightarrow$ $\rightarrow$ motor $\rightarrow$ Inverter $\leftarrow$

Separately excited & shunt

Large no of N

diff

$$\omega_m = \frac{2\pi N_m}{60} \text{ in DC}$$

$$T_a = \frac{P_a}{\omega_m} = \frac{E_a I_a}{\omega_m}$$

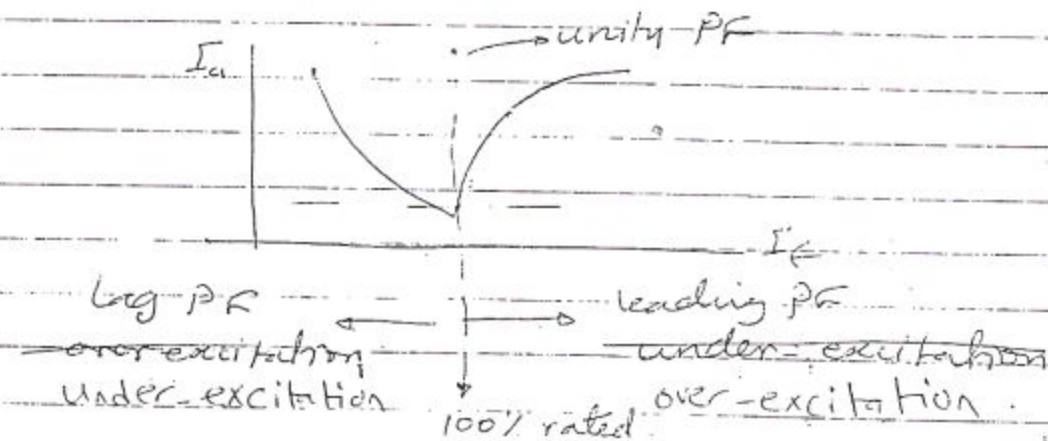
• salient → non of the above

$$E_a = K_a (\phi_f) \cdot \omega_m \quad K_f I_f$$

$$E_a = V_t - I_a R_a$$

$$E_a = V_t - E_a = K \phi \omega = V_t + I_a R_a$$

$$I_{act} = (6-15) I_a(\text{rated})$$



x-axis ? → I_f

y-axis ? → I_a

PF after 100 rated ?

acting over-excited, normally, or under excited?

the connection of the Rotor is Δ , Y , or neither

induction → Δ
synchronous → Y

$$I_o = (1-5) I_{rated}$$

station → Δ or Y is true

$$\text{In SCT} \rightarrow V = (5-13) V_{rated}$$

$R_c = \frac{V_{oc}}{I_{sc}}$ at OCT when $R_c \uparrow$, I_o ??

constant power, Torque, Both

direction of rotation