

-----Uncertainty Analysis-----

$\omega_X = \pm \sqrt{\left(\frac{\partial X}{\partial x_1} \omega_{x_1}\right)^2 + \left(\frac{\partial X}{\partial x_2} \omega_{x_2}\right)^2 + \left(\frac{\partial X}{\partial x_3} \omega_{x_3}\right)^2 + \dots + \left(\frac{\partial X}{\partial x_n} \omega_{x_n}\right)^2}$	$\delta_x = \pm \left(\frac{x_{max} - x_{min}}{2}\right)$
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-----Marcet Boiler-----

$\left(\frac{dP}{dT}\right)_{sat} = \frac{h_{fg}}{T v_{fg}} = \frac{s_{fg}}{v_{fg}}$	$\left(\frac{dP}{dT}\right)_{sat} = \frac{P_{i+1} - P_i}{T_{i+1} - T_i}$	$\left(\frac{dP}{dT}\right)_{sat} = \frac{P_{i+1} - P_{i-1}}{T_{i+1} - T_{i-1}}$	$\left(\frac{dP}{dT}\right)_{sat} = \frac{P_{i-1} - P_i}{T_{i-1} - T_i}$
$\ln\left(\frac{P_2}{P_1}\right)_{sat} \cong \frac{h_{fg1}}{R_{steam}} \left(\frac{1}{T_1} - \frac{1}{T_2}\right) \cong \frac{T_1 s_{fg}}{R_{steam}} \left(\frac{1}{T_1} - \frac{1}{T_2}\right)$	$P = P_{gauge} + P_{atm}$	$T (K) = T (C) + 273.15$	

-----Mechanical Equivalent of Heat-----

$\tau = r g(M + p - m)$	$W = \frac{2\pi r N g \left(M + \frac{p}{1000} - \frac{m}{1000}\right)}{1000}$	$J = \frac{W}{Q}$	$Q = (M C \Delta T)_{drum} + (M C \Delta T)_{water}$
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-----Single Stage Air Compressor-----

$\dot{W}_{m,in} = V * I$	$\dot{W}_{m,out} = \frac{F N_1}{K}, \quad k = 43.41$	$N = \frac{N_1}{3}$	$V_{S_1} = \frac{\pi}{4} d^2 S$
$\dot{W}_{C,in} = \eta_{coupling} * \dot{W}_{m,out}$	$\dot{W}_{C,Isothermal} = \dot{m}_a R_1 T_1 \ln\left(\frac{P_2}{P_1}\right)$	$\dot{W}_{C,Ind} = \bar{P}_m V_{S_1} n_c \left(\frac{N}{60}\right)$	
$\bar{P}_m = \frac{Diagram\ Area}{Diagram\ Length} * 20 \frac{kPa}{mm}$	$\eta_{motor} = \frac{\dot{W}_{m,out}}{\dot{W}_{m,in}}$	$\eta_{isothermal} = \frac{\dot{W}_{C,Isothermal}}{\dot{W}_{C,Ind}}$	$\eta_{vol} = \frac{\dot{m}_a}{\rho_a V_{S_1} n_c \left(\frac{N}{60}\right)}$
$\dot{m}_a = 0.002012 d_o^2 \sqrt{\frac{h_m P_1}{T_1}}$	$\eta_{Mechanical} = \frac{\dot{W}_{C,Isothermal}}{\dot{W}_C}$	$\eta_{Overall} = \frac{\dot{W}_{C,Isothermal}}{\dot{W}_E}$	

-----Flow Through Nozzle-----

$\frac{P^*}{P_0} = \left(\frac{2}{K+1}\right)^{\left(\frac{K}{K-1}\right)}$	$\frac{T^*}{T_0} = \left(\frac{2}{K+1}\right)$	$\frac{\rho^*}{\rho_0} = \left(\frac{2}{K+1}\right)^{\left(\frac{1}{K-1}\right)}$	$M_a = \frac{v}{c}$
$V = \sqrt{\frac{2 K R T_0}{K-1} \left[1 - \left(\frac{P_t}{P_0}\right)^{\left(\frac{K-1}{K}\right)}\right]}$	$\dot{m} = A P_0 \left(\frac{P_t}{P_0}\right)^{\frac{1}{K}} \sqrt{\frac{2 K}{(K-1) R T_0} \left[1 - \left(\frac{P_t}{P_0}\right)^{\left(\frac{K-1}{K}\right)}\right]}$		$C = \sqrt{K R T}$
$\frac{dA}{A} = -\frac{dV}{V} (1 - M_a^2)$	$\frac{dA}{A} = \frac{dP}{\rho V^2} (1 - M_a^2)$	$\frac{dA}{A} = \frac{d\rho}{\rho} \left(\frac{1 - M_a^2}{M_a^2}\right)$	
$\frac{T_o}{T} = 1 + \left(\frac{K-1}{2}\right) M_a^2$	$\frac{P_o}{p} = \left[1 + \left(\frac{K-1}{2}\right) M_a^2\right]^{\left(\frac{K}{K-1}\right)}$	$\frac{\rho_o}{\rho} = \left[1 + \left(\frac{K-1}{2}\right) M_a^2\right]^{\left(\frac{1}{K-1}\right)}$	

-----Specific Heat Ratio for air-----

$\frac{P_2}{P_1} = \left(\frac{P_2}{P_3}\right)^{\frac{K}{K-1}}$	$K = \frac{\ln\left(\frac{P_1}{P_2}\right)}{\ln\left(\frac{P_1}{P_3}\right)}$	$P = \gamma H_m + P_{atm}$	$P_2 = P_{atm}$	$\gamma = \rho g$
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-----Air and Water Heat Pump-----

$\dot{Q}_{cmp} = \dot{m}_w \times C_{p_w} \times (T_6 - T_5)$	$\dot{Q}_{cond} = \dot{m}_w \times C_{p_w} \times (T_7 - T_6)$	$\dot{Q}_T = \dot{Q}_{cmp} + \dot{Q}_{cond}$
$COP_{HP} = \frac{\dot{Q}_{cond}}{W}$	$COP_{HP} = \frac{\dot{Q}_T}{W} = \frac{\dot{Q}_{cond} + \dot{Q}_{cmp}}{W}$	$COP_{HP} = \frac{Q_H}{W} = \frac{\dot{m}_r \times (h_2 - h_3)}{\dot{m}_r \times (h_2 - h_1)} = \frac{(h_2 - h_3)}{(h_2 - h_1)}$

-----Air Cooler and Heat Pump-----			
$\dot{m}_{air} = 0.00105 \sqrt{\frac{H_a P_a}{T_2}}$	$(COP_R)_{max} = \frac{T_L}{T_H - T_L}$	$COP = \frac{\dot{Q}}{\dot{W}_{in}}$	$(COP_{HP})_{max} = \frac{T_H}{T_H - T_L}$
$\dot{Q} = \dot{m}_a (h_{final} - h_{initial})$	$h = h_{dry_air} + \omega h_{vapor}$	$h_{dry_air} = C_{P_{air}} T$	$h_{vapor} = h_g @ (T)$
$(COP_R)_E = \frac{\dot{m}_a [(h_1 - h_2) + (\omega_1 h_{v1} - \omega_2 h_{v2})]}{E_c + E_f}$		$(COP_R)_E = \frac{\dot{m}_a [(h_1 - h_2) + (\omega_1 h_{v1} - \omega_2 h_{v2})] - \dot{m}_c C_{P_w} T_c}{E_c + E_f}$	
$(COP_R)_I = \frac{\dot{m}_a [(h_1 - h_2) + (\omega_1 h_{v1} - \omega_2 h_{v2})] - E_f}{E_c}$		$(COP_R)_{max} = \frac{\left[\frac{(T_1 + T_2)}{2} \right]}{\left[\frac{(T_3 + T_4)}{2} - \frac{(T_1 + T_2)}{2} \right]}$	
$(COP_R)_I = \frac{\dot{m}_a [(h_1 - h_2) + (\omega_1 h_{v1} - \omega_2 h_{v2})] - \dot{m}_c C_{P_w} T_c - E_f}{E_c}$		$(COP_R)_{I\ max} = \frac{T_{10}}{T_6 - T_{10}}$	
$(COP_{HP})_{max} = \frac{\left[\frac{(T_1 + T_2)}{2} \right]}{\left[\frac{(T_1 + T_2)}{2} - \frac{(T_3 + T_4)}{2} \right]}$		$(COP_{HP})_{max} = \frac{T_9}{T_9 - T_8}$	
$(COP_{HP})_E = \frac{\dot{m}_a [(h_2 - h_1) + (\omega_2 h_{v2} - \omega_1 h_{v1})]}{E_c + E_f}$		$(COP_{HP})_I = \frac{\dot{m}_a [(h_2 - h_1) + (\omega_2 h_{v2} - \omega_1 h_{v1})] - E_f}{E_c}$	
-----Refrigeration Unit-----			
$P_s = T \times \omega = F \times r \times \frac{2\pi \times n_c \times 1.98}{60}$		$P_f = F_f \times r \times \frac{2\pi \times n_c \times 1.98}{60}$	$P_i = P_s - P_f$
$P_h(h) = \dot{m}_r \times (h_2 - h_1)$	$\dot{Q}_{rad+conv} = P_s - \dot{m}_r \times (h_2 - h_1)$	$\dot{Q}_{e,1} = \text{Obtained from digital wattmeter}$	
$\dot{Q}_{e,2}(h) = \dot{m}_r \times (h_1 - h_4)$	$\dot{Q}_{c,1} = \dot{m}_w \times C_{pw}(t_6 - t_5)$	$\dot{Q}_{c,2}(h) = \dot{m}_r \times (h_2 - h_3)$	
$COP_{R,act} = \frac{\dot{Q}_L}{\dot{W}_{com}} = \frac{\dot{m}_r \times (h_1 - h_1)}{\dot{m}_r \times (h_2 - h_1)}$			
-----Thermal Power Plants-----			
$\dot{Q}_H = \dot{m}_s(h_{out} - h_{in})$	$\dot{E}_f = \dot{m}_f Q_{cv}$	$\dot{E}_{th} = \dot{m}_f Q_{cv} \eta_c$	
$\eta_{SG} = \frac{\dot{Q}_H}{\dot{E}_{th}}$	$\dot{W}_T = \dot{m}_s(h_{in} - h_{out})$	$\dot{W}_{Shaft} = \tau \omega$	
$\eta_{Coupling} = \frac{\dot{W}_{Shaft}}{\dot{W}_{net}}$	$\dot{W}_E = V I$	$\eta_{Gen} = \frac{\dot{W}_E}{\dot{W}_{Shaft}}$	
$\dot{Q}_L = \dot{m}_s(h_{in} - h_{out})$	$\dot{Q}_{CW} = \dot{m}_{CW}(h_{out} - h_{in})$	$\eta_{Cond} = \frac{\dot{Q}_{CW}}{\dot{Q}_L}$	
$\dot{W}_p = \dot{m}_s(h_{in} - h_{out})$	$\dot{W}_{net} = \dot{W}_T - \dot{W}_p$	$\eta_{max} = 1 - \frac{T_L}{T_H}$	
-----Revision on Air-Vapor Mixture and Psychrometry-----			
$H = H_a + H_v = m_a h_a + m_v h_v$		$\omega = \frac{m_v}{m_a} = 0.622 \frac{P_v}{P_a} = \frac{0.622 P_v}{P - P_v}$	$\Phi = \frac{m_v}{m_g} = \frac{P_v}{P_g}$
$\Phi = \frac{\omega P}{(0.622 + \omega) P_g}$	$\omega = \frac{0.622 \Phi P_g}{P - \Phi P_g}$	$h = h_a + \omega h_g$	$\dot{V} = \dot{m}_a v$
$h_v(T, Low P) \cong h_g(T) = 2500.9 + 1.82 T \quad T \text{ is in } C$		$P_g = P_{sat} @ T$	$T_{dp} = T_{sat} @ P_v$
$\dot{Q} = \dot{m}_a (\Delta h) \quad \text{for Simple Heating or Simple Cooling}$		$\dot{m}_w = \dot{m}_a (\omega_f - \omega_i)$	
$\dot{Q} = \dot{m}_a (\Delta h) - \dot{m}_w h_w \quad \text{for cooling with Dehumidification;}$			